

PROPAGATION AND REFLECTION OF MAGNETO-ELASTIC PLANE WAVES AT THE FREE SURFACE OF A ROTATING MICROPOLAR FIBRE-REINFORCED MEDIUM WITH VOIDS

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This work investigates rotational effects on propagation and reflection of waves at the free surface of a micropolar fibre-reinforced medium with voids under magnetic fields. When the P-wave is incident on the free surface, there exist four coupled reflected plane waves traveling in the medium; quasi-longitudinal displacement (qLD) wave, quasi-transverse displacement (qTD) wave, quasi-transverse microrotational (qTM) wave and a wave due to voids. Normal mode analysis is adopted in concomitant with Snell's laws, and appropriate boundary conditions in determination of the solution. Amplitude ratios which correspond to reflected waves in vertical and horizontal components are presented analytically and graphically.

Keywords: rotation, micropolar fibre-reinforced, voids, reflection coefficients, magnetic field

1. Introduction

Fibre-reinforced composite materials and their analysis of stress and deformation are of great interest to researchers in solid mechanics. This is as a result of its weightlessness and high tensile strength. Structural designers mostly in the field of engineering, science and technology, usually sought after such type of materials. However, many researchers have investigated wave propagation in various materials or media. But a particular investigation of isotropic generalized solids with voids paved way as an evidence to the existence of new or transformed waves, whose importance to seismologists in improving earthquake estimations cannot be over emphasized. In geophysics, for instance, the reflection and refraction of seismic waves gave credence to researchers to investigate the earth's interior and structures. Thus, it is obvious that most large bodies such as planets, moon and earth possess angular velocity. Consequently, this necessitates the study of rotational effects on reflection of plane waves. Moreover, the frame of reference of rotation of the medium, centrifugal acceleration and Coriolis effects are taken into considerations in the equation of motion.

On the other hand, micro-continuum as a material property due to deformation consists of microstretch, micropolar and micromorphic theories, and this depends on the order to which the micro-degree is incorporated. Eringen (1967) developed theory from micropolar elasticity to micropolar linear constitutive theories with internal friction. McCarthy and Eringen (1969) investigated the problem on micropolar viscoelastic waves. Kumar *et al.* (1990) studied problems associated with Lamb's plane micropolar viscoelastic medium with stretch. Biswas *et al.* (1996) studied the axisymmetric Lamb's problem of a micropolar viscoelastic medium. Singh and Kumar (1998) investigated the amplitude ratios of reflection and refraction of plane waves between a micropolar elastic solid and viscoelastic solid interfaces. Singh (2000) developed the reflection/transmission between a liquid and micro-polar viscoelastic solid interfaces with stretch. Nunziato and Cowin (1979) and Cowin and Nunziato (1983) discussed both linear and nonlinear

theories of elastic porous media. Puri and Cowin (1985) studied the effects of voids on plane waves in linear elastic media. Singh (2017) gave account of reflection of elastic plane surface waves of a half-space with impedance boundary conditions. Sengupta and Nath (2001) discussed surface waves in fibre-reinforced media. Chattopadhyay *et al.* (2002) studied reflection of quasi-SV and quasi-P waves using both free and rigid boundary conditions of a fibre-reinforced medium. Chaudhary *et al.* (2004) envisaged reflection/transmission of plane waves between self-reinforced two elastic half-spaces. Khan *et al.* (2015) studied the effects of surface waves under the influence of gravity in a non-homogeneous fibre-reinforced media with voids. Tauchert (1971) investigated thermal stresses in micropolar elastic solids. Chattopadhyay and Choudhury (1990) obtained results on propagation, reflection/transmission of waves under the magnetic effects in a self-reinforced medium. Kumar *et al.* (2015) worked on reflection of plane waves in transversely isotropic micropolar viscoelastic media with thermal effects. Furthermore, Abd-Alla *et al.* (2017) investigated rotational behavior of magneto-thermoelastic surface waves in fibre-reinforced viscoelastic media of higher order. Lata (2018) studied reflection and refraction of plane waves in a layered nonlocal elastic and anisotropic thermoelastic medium. Schoenberg and Censor (1973) examined the propagation of waves in a rotating, homogeneous, isotropic, linear elastic medium. An eigenvalue approach was utilized by Sinha and Bera (2003) to solve the fundamental equations of problems of generalized thermoelasticity with one relaxation parameter including the heat source in an infinite rotating medium. Sunita *et al.* (2019) examined reflection on a free surface of a fibre-reinforced thermoelastic rotating medium with two-temperature and phase-lag. Roy *et al.* (2017), examined propagation and reflection of plane waves in a rotating magneto-elastic fibre-reinforced semi space with surface stress. Hillion (2008) investigated harmonic plane wave propagation in anisotropic chiral media.

In the light of the above literature, the current study envisages propagation and reflection of magneto-elastic plane waves at free surfaces of a rotating micropolar fibre-reinforced medium with porosity under magnetic fields. That is, interactions between the magnetic field and the rotating micropolar fibre-reinforced medium with voids or porosity in the x_1x_2 -plane is considered. Due to micropolarity, the coefficient matrices in the constituent relations are non-symmetric i.e., the stress tensors and deformation tensors are considered to be non-symmetric. Thus, the micropolar fibre-reinforced problem in 2-D is modelled. The governing equations are solved by using free boundary conditions also called natural boundary conditions. We observed that four reflected waves exist when, in particular, the P-wave is incident on the free surface or at the boundary $x_2 = 0$; quasi-longitudinal displacement (qLD) or P-wave, quasi-transverse displacement (qTD) or SV-wave, quasi-transverse microrotational (qTM) wave and a wave due to voids. Amplitude ratios or reflection coefficients which correspond to the reflected waves in both horizontal and vertical components are presented analytically. Also, by using Mathematica software, computational results which stipulate the effects of rotation, magnetic field, fibre-reinforced and voids parameters for the horizontal reflection coefficients are shown graphically. Some particular results can also be deduced in the absence of rotation, magnetic field and fibre-reinforced parameters, yielding the results of a micropolar isotropic solid with voids.

2. Formulation of the problem

The basic field relations for a micro-polar fibre-reinforced homogenous linearly elastic anisotropic medium with the reinforcement direction \mathbf{a} and voids (Eringen, 1967; Kumar *et al.*, 2015; Lakes and Benedict, 1982; Cowin and Nunziato, 1983) are specified by

$$\sigma_{ij} = B_{ijmn}E_{mn} + N_{ijmn}\psi_{mn} + \xi\phi\delta_{ij} \quad m_{ij} = B_{jimn}E_{mn} + N_{mnji}\psi_{mn} \quad (2.1)$$

The deformations and wryness tensors are taken as

$$E_{ij} = u_{j,i} + \varepsilon_{jim}\phi_m^* \quad \psi_{mn} = \phi_{m,n}^* \quad i = j = m = n = 1, 2, 3 \quad (2.2)$$

The balance laws in the presence of rotation, magnetic fields and voids (Abd-Alla *et al.*, 2017; Eringen, 1967; Cowin and Nunziato, 1983) are written below

$$\begin{aligned}
 \sigma_{ij,i} + F_j &= \rho(\ddot{u}_j + \Omega_i u_i \Omega_j - \Omega^2 u_j + 2\varepsilon_{jik} \Omega_i \dot{u}_k) \\
 m_{ij,i} + \varepsilon_{jmn} \sigma_{mn} &= \rho J \dot{\phi}_j^* \\
 \xi_1(\phi_{,ii}) - \omega_0 \phi - \varpi \dot{\phi} - \xi(u_{i,i}) &= \rho \kappa \ddot{\phi}
 \end{aligned} \tag{2.3}$$

Let the solid medium be rotating about the x_3 -axis with uniform angular velocity Ω , i.e. $\Omega = \Omega(0, 0, 1)$, where σ_{ij} [N/m²], m_{ij} [N/m²], ϕ_j^* , u_j [m] and ϕ are the stress tensor, couple stresses, microrotation vector, displacement vector and volume fraction field, respectively. Also, ρ , ξ and J [m²] represent the bulk mass density, void parameter and micronertia respectively. B_{ijmn} , B_{jimn} and N_{ijmn} are characteristic constants of the material, and also non symmetric properties of B_{ijmn} , B_{jimn} and N_{ijmn} hold. For simplicity, we chose $\mathbf{a} = [a_1, a_2, a_3]$ such that $\mathbf{a} = [1, 0, 0]$ as the fibre direction. δ_{ij} is the Kronecker-delta function, ε_{jim} is the Levi-Civita alternating symbol or tensor. The index after comma represents partial derivative with respect to coordinate and the superscript dot specifies partial derivative with respect to time. Consider deformation in the x_1x_2 -plane and the microrotation vector as $\phi^* = [0, 0, \phi_3^*]$. Also Einstein summation convention over repeated indexes is used. However, $F_i = \mu_0 \varepsilon_{ijk} J_j H_k$ and we take the linearized Maxwell equations governing the electromagnetic field for a perfectly conducting medium as

$$\begin{aligned}
 \varepsilon_{ijk} H_{k,j} &= \varepsilon_0 \varepsilon_{ijk} J_j \dot{E}_k & \varepsilon_{ijk} E_{k,j} &= -\mu_0 \dot{H}_i & H_{i,i} &= 0 \\
 E_{i,i} &= 0 & E_i &= \mu_0 \varepsilon_{ijk} \dot{u}_j H_k
 \end{aligned}$$

where $H_i = H_0 \delta_{i3} + h_i$, h_i is the induced magnetic field and ε_0 is electric permeability in farads/meters [F/m], and the material lies in the x_1x_2 -plane. Thus, $H_i = H_0 \delta_{i3} + h_i$. Then the magnetic force is given as follows: $F_i = \mu_0 H_0^2 (e_{,i} - \varepsilon_0 \mu_0 \ddot{u}_i)$, $F_3 = 0$ and $h_i(x_1, x_2, x_3) = -u_{k,k} \delta_{i3}$, where $e = u_{1,1} + u_{2,2}$. In these equations, F_i represents the magnetic force in newtons [N], J_i is the current density in A/m², H_i is the magnetic field vector having SI unit as ampere per meter [A/m], and μ_0 is magnetic permeability, measured in henry per metre [H/m]. Considering the fact that the tensors are non-symmetric, Eqs. (2.3) in the component form can be written as follows

$$\begin{aligned}
 B_1 u_{1,11} + (B_2 + B_3) u_{2,12} + B_4 u_{1,22} + B_1^* \phi_{3,2}^* + \xi \phi_{,1} &= \varepsilon_0 \mu_0^2 H_0^2 \ddot{u}_1 + \rho(\ddot{u}_1 - \Omega^2 u_1 - 2\dot{u}_2 \Omega) \\
 B_5 u_{2,11} + B_2 u_{1,12} + B_6 u_{2,22} - B_5 \phi_{3,1}^* + \xi \phi_{,2} &= \varepsilon_0 \mu_0^2 H_0^2 \ddot{u}_2 + \rho(\ddot{u}_2 - \Omega^2 u_2 + 2\dot{u}_1 \Omega) \\
 B_5 \phi_{3,11}^* + B_4 \phi_{3,22}^* - 2B_4 \phi_3^* + B_4(u_{2,1} - u_{1,2}) &= \rho J \dot{\phi}_3^* \\
 \xi_1(\phi_{,11} + \phi_{,22}) - \omega_0 \phi - \varpi \dot{\phi} - \xi(u_{1,1} + u_{2,2}) &= \rho \kappa \ddot{\phi}
 \end{aligned} \tag{2.4}$$

where

$$\begin{aligned}
 B_1 &= \lambda + \beta + 2\alpha - 2\mu_T + 4\mu_L + \mu_0 H_0^2 & B_2 &= \lambda + \alpha + \mu_0 H_0^2 \\
 B_3 &= 2(\mu_L - \mu_T) & B_4 &= 2\mu_T & B_5 &= 2\mu_L \\
 B_6 &= \lambda + 2\mu_T + \mu_0 H_0^2 & B_1^* &= B_4 - B_3
 \end{aligned} \tag{2.5}$$

Also λ represents Lamé's material constant, α , β and $(\mu_L - \mu_T)$ are the fibre-reinforced parameters. All these parameters define the anisotropic model. If we consider $\mu_L = \mu_T = \mu$ (Lamé's constant) and $\alpha = \beta = 0$, the simple isotropic case is achieved.

3. Normal modes analysis and solution of the problem

Consider a rotating homogeneous micropolar fibre-reinforced anisotropic magneto-elastic medium with voids occupying the half-space $x_2 \leq 0$ under the influence of a magnetic field. And

let the plane waves be incident at the free boundary $x_2 = 0$ at an angle θ with the x_2 -axis. Let the normal mode analysis be applicable such that the incident waves have the following displacements chosen as

$$\{u_j, \phi^*, \phi\} = \{R, P, \phi_0^*, \phi_0\} e^{i[k(x_1 \sin \theta + x_2 \cos \theta) - \omega t]} \quad j = 1, 2 \quad (3.1)$$

where R , P , ϕ_0^* and ϕ_0 are amplitudes of u_1 , u_2 , ϕ_3^* and ϕ , measured in meters, respectively. ω is the angular velocity in radians per second, $c = \omega/k$ is the phase velocity of the wave in meter per second, and k is the wave number and $(\sin \theta, \cos \theta)$ represents the projection of waves normal onto the x_1x_2 -plane. We make use of Eq. (3.1) into Eqs. (2.4), respectively, which yields

$$\begin{aligned} & \left\{ D_1 - \left[\frac{\Omega^2}{k^2} \rho + c^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho) \right] \right\} R + \left[(B_2 + B_3) \cos \theta \sin \theta + 2ic \frac{\Omega}{k} \rho \right] \\ & \quad - i \left(B_1^* \frac{1}{k} \cos \theta \right) \phi_0^* - i \left(\xi \frac{1}{k} \sin \theta \right) \phi_0 = 0 \\ & \left(B_2 \cos \theta \sin \theta - 2ic \frac{\Omega}{k} \rho \right) R + \left\{ D_2 - \left[\frac{\Omega^2}{k^2} \rho + c^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho) \right] \right\} P \\ & \quad + i \left(B_5 \frac{1}{k} \sin \theta \right) \phi_0^* - i \left(\xi \frac{1}{k} \cos \theta \right) \phi_0 = 0 \\ & (ikB_4 \cos \theta) R - (ikB_4 \sin \theta) P + (k^2 D_3 + 2B_4 - Jk^2 \rho c^2) \phi_0^* = 0 \\ & (i\xi k \sin \theta) R + (i\xi k \cos \theta) P + (\xi_1 k^2 + \omega_0 - \varpi i k c - \rho \kappa k^2 c^2) \phi_0 = 0 \end{aligned} \quad (3.2)$$

where $D_1 = B_1 \sin^2 \theta + B_4 \cos^2 \theta$, $D_2 = B_5 \sin^2 \theta + B_6 \cos^2 \theta$, and $D_3 = B_5 \sin^2 \theta + B_4 \cos^2 \theta$. For a non-trivial solution, Eqs. (3.2) becomes the quartic equation as follows

$$r^4 + H_1 r^3 + H_2 r^2 + H_3 r + H_4 = 0 \quad (3.3)$$

where $r = c^2$ which means that characteristic Eq. (3.3) with complex material coefficients H_1 , H_2 , H_3 and H_4 , yields four distinct complex roots; detailing that four waves propagate, with complex phase velocities c_1 , c_2 , c_3 and c_4 corresponding to the wave numbers k_1 , k_2 , k_3 and k_4 , respectively. So this means that the two dimensional model of reflection and propagation of magneto-elastic plane waves in a rotating micropolar fibre-reinforced half space medium with voids under consideration have four reflected waves; quasi-P wave, quasi-SV wave, quasi-transverse microrotational wave and a wave due to voids travelling in the medium, if we assume that anyone of the four waves is incident at the free surface of the material.

4. Reflection of plane waves at the free surface

We consider the case when the quasi-P wave (A_0) is incident at the boundary $x_2 = 0$ of the rotating micropolar fibre-reinforced anisotropic semi-infinite medium with voids under the influence of magnetic fields. Then, there exists four coupled reflected waves as the quasi-P (A_1), quasi-SV (A_2), quasi-TM (A_3) and due to void (A_4), see Fig. 1.

Thus, the total displacements can be assumed in the following form

$$\{u_1, u_2, \phi_3^*, \phi\} = \sum_{l=0}^4 \{R_l, P_l, \phi_0^*, \phi_0\} e^{id_l} \quad (4.1)$$

where

$$\begin{aligned} d_0 &= k_0 [x_1 \sin(e) + x_2 \cos(e) - c_1 t] & d_1 &= k_1 [x_1 \sin(e) - x_2 \cos(e) - c_1 t] \\ d_2 &= k_2 [x_1 \sin(f) - x_2 \cos(f) - c_2 t] & d_3 &= k_3 [x_1 \sin(g) - x_2 \cos(g) - c_3 t] \\ d_4 &= k_4 [x_1 \sin(h) - x_2 \cos(h) - c_4 t] \end{aligned}$$

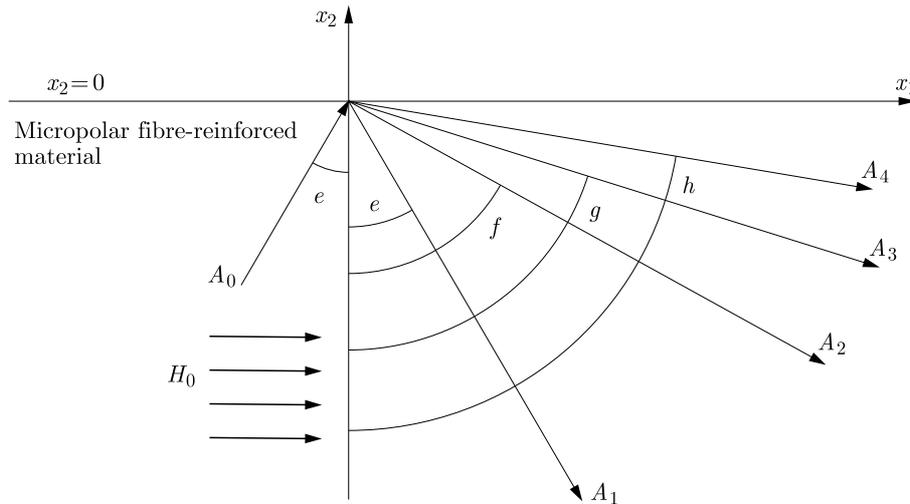


Fig. 1. Schematic of the problem showing incident and reflected waves

and R_0 is the amplitude of the incident wave while R_l , $l = 1, 2, 3, 4$, are amplitudes of the reflected waves in the horizontal components. Similarly, P_0 is the amplitude of the incident wave in the vertical components while P_l , $l = 1, 2, 3, 4$ are amplitudes of reflected waves in the vertical components. Incident and reflected waves given by (4.1) must satisfy equations of motion (2.4)_{1,2} as a result of the consistency condition; following (Roy *et al.*, 2017; Baljeet and Sarva, 2004), Eq. (2.4)₁ becomes

$$\begin{aligned}
 & [D_1(e) - l_1]R_0 + \left[(B_2 + B_3) \sin(e) \cos(e) + 2ic_1 \frac{\Omega}{k_1} \rho \right] P_0 \\
 & \quad - i \left[\frac{i}{k_0} B_1^* \cos(e) \right] \phi_0^* - \left[\frac{i}{k_0} \xi \sin(e) \right] \phi_0 = 0 \\
 & [D_1(e) - l_1]R_1 - \left[(B_2 + B_3) \sin(e) \cos(e) - 2ic_1 \frac{\Omega}{k_1} \rho \right] P_1 \\
 & \quad - i \left[\frac{i}{k_1} B_1^* \cos(e) \right] \phi_0^* - \left[\frac{i}{k_1} \xi \sin(e) \right] \phi_0 = 0 \\
 & [D_1(f) - l_2]R_2 - \left[(B_2 + B_3) \sin(f) \cos(f) - 2ic_2 \frac{\Omega}{k_2} \rho \right] P_2 \\
 & \quad - i \left[\frac{i}{k_2} B_1^* \cos(f) \right] \phi_0^* - \left[\frac{i}{k_2} \xi \sin(f) \right] \phi_0 = 0 \\
 & [D_1(g) - l_3]R_3 - \left[(B_2 + B_3) \sin(g) \cos(g) - 2ic_3 \frac{\Omega}{k_3} \rho \right] P_3 \\
 & \quad - i \left[\frac{i}{k_3} B_1^* \cos(g) \right] \phi_0^* - \left[\frac{i}{k_3} \xi \sin(g) \right] \phi_0 = 0 \\
 & [D_1(h) - l_4]R_4 - \left[(B_2 + B_3) \sin(h) \cos(h) - 2ic_4 \frac{\Omega}{k_4} \rho \right] P_4 \\
 & \quad - i \left[\frac{i}{k_4} B_1^* \cos(h) \right] \phi_0^* - \left[\frac{i}{k_4} \xi \sin(h) \right] \phi_0 = 0
 \end{aligned} \tag{4.2}$$

Equation (4.2) is made possible using Snell's law such that: $c_1 k_0 = c_1 k_1 = c_2 k_2 = c_3 k_3 = c_4 k_4$ and also $k_0 \sin(e) = k_1 \sin(e) = k_2 \sin(f) = k_3 \sin(g) = k_4 \sin(h)$. Observe that $k_0 = k_1$ and c_i , $i = 1, 2, 3, 4$, are functions of material parameters. We can rewrite Eq. (4.2) as follows

$$\begin{aligned}
R_0 &= -b_1 P_0 + b_2 \phi_0^* + b_3 \phi_0 & R_1 &= b_1 P_1 + b_4 \phi_0^* + b_5 \phi_0 \\
R_2 &= b_6 P_2 + b_7 \phi_0^* + b_8 \phi_0 & R_3 &= b_9 P_3 + b_{10} \phi_0^* + b_{11} \phi_0 \\
R_4 &= b_{12} P_4 + b_{13} \phi_0^* + b_{14} \phi_0
\end{aligned} \tag{4.3}$$

where

$$\begin{aligned}
b_1 &= \frac{(B_2 + B_3) \sin(e) \cos(e) + (2ic_1 \Omega \rho)/k_1}{D_1(e) - l_1} & b_2 &= \frac{iB_1^* \cos(e)}{k_0[D_1(e) - l_1]} \\
b_3 &= \frac{i\xi \sin(e)}{k_0[D_1(e) - l_1]} & b_4 &= \frac{i\xi B_1^* \cos(e)}{k_1[D_1(e) - l_1]} & b_5 &= \frac{i\xi \sin(e)}{k_1[D_1(e) - l_1]} \\
b_6 &= \frac{(B_2 + B_3) \sin(f) \cos(f) - (2ic_2 \Omega \rho)/k_2}{D_1(f) - l_2} & b_7 &= \frac{iB_1^* \cos(f)}{k_2[D_1(f) - l_2]} \\
b_8 &= \frac{i\xi \sin(f)}{k_2[D_1(f) - l_2]} & b_9 &= \frac{(B_2 + B_3) \sin(g) \cos(g) - (2ic_3 \Omega \rho)/k_3}{D_1(g) - l_3} \\
b_{10} &= \frac{iB_1^* \cos(g)}{k_3[D_1(g) - l_3]} & b_{11} &= \frac{i\xi \sin(g)}{k_3[D_1(g) - l_3]} \\
b_{12} &= \frac{(B_2 + B_3) \sin(h) \cos(h) - (2ic_4 \Omega \rho)/k_4}{D_1(h) - l_4} & b_{13} &= \frac{iB_1^* \cos(h)}{k_4[D_1(h) - l_4]} \\
b_{14} &= \frac{i\xi \sin(h)}{k_4[D_1(h) - l_4]} & l_1 &= \frac{\Omega^2}{k_1^2} \rho + c_1^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho) \\
l_2 &= \frac{\Omega^2}{k_2^2} \rho + c_2^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho) & l_3 &= \frac{\Omega^2}{k_3^2} \rho + c_3^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho) \\
l_4 &= \frac{\Omega^2}{k_4^2} \rho + c_4^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho)
\end{aligned}$$

4.1. Free boundary conditions at the surface of the medium

We consider a free surface boundary at $x_2 = 0$ of the micropolar fibre-reinforced rotating semi-infinite medium permeated by a uniform magnetic field with voids, i.e.: $\sigma_{i2} + \bar{\sigma}_{i2} = 0$, $i = 1, 2$, $m_{23} = 0$, and $\phi_{,2} = 0$ at $x_2 = 0$. Maxwell's stresses (Abd-Alla *et al.*, 2017) are

$$\bar{\sigma}_{ij} = \mu_0 H_0 (H_i h_j + H_j h_i - H_k h_k \delta_{ij}) \Rightarrow \bar{\sigma}_{ij} = \mu_0 H_0 \begin{vmatrix} -h_3 & 0 & h_1 \\ 0 & -h_3 & h_2 \\ h_1 & h_2 & h_3 \end{vmatrix}$$

$$h_3 = -H_0(u_{1,1} + u_{2,2})h_1 = h_2 = 0$$

and

$$\begin{aligned}
\text{for } i = 1 : \quad \sigma_{12} + \bar{\sigma}_{12} = 0 \quad \text{but} \quad \bar{\sigma}_{12} = 0 \Rightarrow \sigma_{12} = 0 \\
\text{for } i = 2 : \quad \sigma_{22} + \bar{\sigma}_{22} = 0 \Rightarrow \sigma_{22} + \mu_0 H_0^2 (u_{1,1} + u_{2,2}) = 0 \\
m_{23} = 0 \Rightarrow \phi_{3,2}^* = 0 \quad \phi_{,2} = 0
\end{aligned} \tag{4.4}$$

Thus, from equation (4.3), we obtain the ratio

$$\begin{aligned}
\frac{R_1}{R_0} &= \frac{1}{\varsigma} \left(\frac{b_1 P_1}{P_0} + \frac{b_4 \phi_0^*}{P_0} + \frac{b_5 \phi_0}{P_0} \right) & \frac{R_2}{R_0} &= \frac{1}{\varsigma} \left(\frac{b_6 P_2}{P_0} + \frac{b_7 \phi_0^*}{P_0} + \frac{b_8 \phi_0}{P_0} \right) \\
\frac{R_3}{R_0} &= \frac{1}{\varsigma} \left(\frac{b_9 P_3}{P_0} + \frac{b_{10} \phi_0^*}{P_0} + \frac{b_{11} \phi_0}{P_0} \right) & \frac{R_4}{R_0} &= \frac{1}{\varsigma} \left(\frac{b_{12} P_4}{P_0} + \frac{b_{13} \phi_0^*}{P_0} + \frac{b_{14} \phi_0}{P_0} \right) \\
\varsigma &= \frac{b_2 \phi_0^*}{P_0} + \frac{b_3 \phi_0}{P_0} - b_1
\end{aligned} \tag{4.5}$$

and also by using Eqs. (4.4), we have

$$\begin{aligned}
 (a_{11}P_1 + a_{12}P_2 + a_{13}P_3 + a_{14}P_4) \frac{1}{P_0} &= a_{15} \\
 (a_{21}P_1 + a_{22}P_2 - a_{23}P_3 + a_{24}P_4) \frac{1}{P_0} &= -a_{25} \\
 (a_{31}P_1 - a_{32}P_2 + a_{33}P_3 + a_{34}P_4) \frac{1}{P_0} &= -a_{35} \\
 (a_{41}P_1 + a_{42}P_2 + a_{43}P_3 - a_{44}P_4) \frac{1}{P_0} &= a_{45}
 \end{aligned}
 \tag{4.6}$$

where

$$\begin{aligned}
 a_{11} &= k_1 \sin(e) & a_{12} &= k_2 \sin(f) & a_{13} &= k_3 \sin(g) & a_{14} &= k_4 \sin(h) \\
 a_{15} &= -k_0 \sin(e) - \frac{i\phi_0^*}{P_0} & a_{21} &= [L_1 b_1 \sin(e) - L_2 \cos(e)]k_1 \\
 a_{22} &= [L_1 b_6 \sin(f) - L_2 \cos(f)]k_2 & a_{23} &= -[L_1 b_9 \sin(g) - L_2 \cos(g)]k_3 \\
 a_{24} &= [L_1 b_{12} \sin(h) - L_2 \cos(h)]k_4 \\
 a_{25} &= -[L_1 b_1 \sin(e) - L_2 \cos(e)]k_0 - L_1 \left\{ \left(b_2 \frac{\phi_0^*}{P_0} + b_3 \frac{\phi_0}{P_0} \right) k_0 \sin(e) \right. \\
 &\quad + \left(b_4 \frac{\phi_0^*}{P_0} + b_5 \frac{\phi_0}{P_0} \right) k_1 \sin(e) + \left(b_7 \frac{\phi_0^*}{P_0} + b_8 \frac{\phi_0}{P_0} \right) k_2 \sin(f) + \left(b_{10} \frac{\phi_0^*}{P_0} + b_{11} \frac{\phi_0}{P_0} \right) k_3 \sin(g) \\
 &\quad \left. + \left(b_{13} \frac{\phi_0^*}{P_0} + b_{14} \frac{\phi_0}{P_0} \right) k_4 \sin(h) \right\} + i\xi \frac{\phi_0}{P_0} \\
 a_{31} &= -B_1 b_1 a_{11}^2 + (B_2 + B_3) a_{11} k_1 \cos(e) + 2i\rho c_1 k_1 \Omega - B_4 b_1 k_1^2 \cos^2(e) \\
 &\quad + [\Omega^2 \rho + c_1^2 k_1^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho)] b_1 \\
 a_{32} &= -\{ -B_1 b_6 a_{12}^2 + (B_2 + B_3) a_{12} k_2 \cos(f) + 2i\rho c_2 k_2 \Omega - B_4 b_6 k_2^2 \cos^2(f) \\
 &\quad + [\Omega^2 \rho + c_2^2 k_2^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho)] b_6 \} \\
 a_{33} &= -B_1 b_9 a_{13}^2 + (B_2 + B_3) a_{13} k_3 \cos(g) + 2i\rho c_3 k_3 \Omega - B_4 b_9 k_3^2 \cos^2(g) \\
 &\quad + [\Omega^2 \rho + c_3^2 k_3^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho)] b_9 \\
 a_{34} &= -B_1 b_{12} a_{14}^2 + (B_2 + B_3) a_{14} k_4 \cos(h) + 2i\rho c_4 k_4 \Omega - B_4 b_{12} k_4^2 \cos^2(h) \\
 &\quad + [\Omega^2 \rho + c_4^2 k_4^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho)] b_{12} \\
 a_{35} &= -\left\{ B_1 \left[\left(-b_1 + b_2 \frac{\phi_0^*}{P_0} + b_3 \frac{\phi_0}{P_0} \right) k_0^2 \sin^2(e) + \left(b_4 \frac{\phi_0^*}{P_0} + b_5 \frac{\phi_0}{P_0} \right) a_{11}^2 + \left(b_7 \frac{\phi_0^*}{P_0} + b_8 \frac{\phi_0}{P_0} \right) a_{12}^2 \right. \right. \\
 &\quad + \left. \left(b_{10} \frac{\phi_0^*}{P_0} + b_{11} \frac{\phi_0}{P_0} \right) a_{13}^2 + \left(b_{13} \frac{\phi_0^*}{P_0} + b_{14} \frac{\phi_0}{P_0} \right) a_{14}^2 \right] + (B_2 + B_3) k_0^2 \cos^2(e) + 2i\rho c_1 \Omega \\
 &\quad + B_4 \left[\left(-b_1 + b_2 \frac{\phi_0^*}{P_0} + b_3 \frac{\phi_0}{P_0} \right) k_0^2 \cos^2(e) + \left(b_4 \frac{\phi_0^*}{P_0} + b_5 \frac{\phi_0}{P_0} \right) k_1^2 \cos^2(e) \right. \\
 &\quad + \left. \left(b_7 \frac{\phi_0^*}{P_0} + b_8 \frac{\phi_0}{P_0} \right) k_2^2 \cos^2(f) + \left(b_{10} \frac{\phi_0^*}{P_0} + b_{11} \frac{\phi_0}{P_0} \right) k_3^2 \cos^2(g) \right. \\
 &\quad + \left. \left(b_{13} \frac{\phi_0^*}{P_0} + b_{14} \frac{\phi_0}{P_0} \right) k_4^2 \cos^2(h) \right] - \left(-b_1 + b_2 \frac{\phi_0^*}{P_0} + b_3 \frac{\phi_0}{P_0} \right) [\Omega^2 \rho + c_1^2 k_0^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho)] \\
 &\quad - \left(b_4 \frac{\phi_0^*}{P_0} + b_5 \frac{\phi_0}{P_0} \right) [\Omega^2 \rho + c_1^2 k_1^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho)] - \left(b_7 \frac{\phi_0^*}{P_0} + b_8 \frac{\phi_0}{P_0} \right) [\Omega^2 \rho + c_2^2 k_2^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho)] \\
 &\quad - \rho \left(b_{10} \frac{\phi_0^*}{P_0} + b_{11} \frac{\phi_0}{P_0} \right) [\Omega^2 \rho + c_3^2 k_3^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho)] \\
 &\quad \left. - \rho \left(b_{13} \frac{\phi_0^*}{P_0} + b_{14} \frac{\phi_0}{P_0} \right) [\Omega^2 \rho + c_4^2 k_4^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho)] - i\xi \frac{\phi_0}{P_0} [k_0 \sin(e) + a_{11} + a_{12} + a_{13} + a_{14}] \right\}
 \end{aligned}$$

$$\begin{aligned}
a_{41} &= -(B_5 + B_6)a_{11}^2 + [B_2a_{11}k_1 \cos(e) - 2i\rho c_1 k_1 \Omega]b_1 + \Omega^2 \rho + c_1^2 k_1^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho) \\
a_{42} &= -(B_5 + B_6)a_{12}^2 + [B_2a_{12}k_2 \cos(f) - 2i\rho c_2 k_2 \Omega]b_6 + \Omega^2 \rho + c_2^2 k_2^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho) \\
a_{43} &= -(B_5 + B_6)a_{13}^2 + [B_2a_{13}k_3 \cos(g) - 2i\rho c_3 k_3 \Omega]b_9 + \Omega^2 \rho + c_3^2 k_3^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho) \\
a_{44} &= -\{-(B_5 + B_6)a_{14}^2 + [B_2a_{14}k_4 \cos(h) - 2i\rho c_4 k_4 \Omega]b_{12} + \Omega^2 \rho + c_4^2 k_4^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho)\} \\
a_{45} &= [B_5 \sin^2(e) + B_6 \cos^2(e)]k_0^2 - \Omega^2 \rho + c_1^2 k_0^2 (\varepsilon_0 \mu_0^2 H_0^2 + \rho) \\
&+ \left(b_2 \frac{\phi_0^*}{P_0} + b_3 \frac{\phi_0}{P_0}\right)[B_2 k_0^2 \cos(e) \sin(e) - 2i\rho c_1 k_1 \Omega] \\
&- \left(b_4 \frac{\phi_0^*}{P_0} + b_5 \frac{\phi_0}{P_0}\right)[k_1 B_2 a_{11} \cos(e) - 2i\rho c_1 k_1 \Omega] \\
&- \left(b_7 \frac{\phi_0^*}{P_0} + b_8 \frac{\phi_0}{P_0}\right)[k_2 B_2 a_{12} \cos(f) - 2i\rho c_2 k_2 \Omega] \\
&- \left(b_{10} \frac{\phi_0^*}{P_0} + b_{11} \frac{\phi_0}{P_0}\right)[B_2 k_3 a_{13} \cos(g) - 2i\rho c_3 k_3 \Omega] \\
&- \left(b_{13} \frac{\phi_0^*}{P_0} + b_{14} \frac{\phi_0}{P_0}\right)[k_4 B_2 a_{15} \cos(h) - 2i\rho c_4 k_4 \Omega] \\
&+ iB_5 \frac{\phi_0^*}{P_0} [k_0 \sin(e) + a_{11} + a_{12} + a_{13} + a_{14}] \\
L_1 &= B_2 \quad L_2 = B_6
\end{aligned}$$

Equation (4.6) can be solved for P_i/P_0 , $i = 1, 2, 3, 4$ using Cramer's rule or any solver. $W_i = |P_i/P_0|$, $i = 1, 2, 3, 4$, give the amplitude ratios along the vertical reflection component. Hence, the amplitude ratios $Z_i = |R_i/R_0|$, $i = 1, 2, 3, 4$, along the horizontal reflection component can be obtained from Eqs. (4.5) by substituting the values of P_i/P_0 , $i = 1, 2, 3, 4$.

5. Computational results and discussion

The effects of rotation, reinforcement and voids parameters on reflection coefficients of plane waves in the micropolar fibre-reinforced material under the influence of a magnetic field are studied by considering the following numerical physical constants (Othman and Lotfy, 2013) and other parameters as: $\lambda = 7.59 \cdot 10^9 \text{ N/m}^2$, $\mu_T = 1.89 \cdot 10^9 \text{ N/m}^2$, $\mu_L = 2.45 \cdot 10^9 \text{ N/m}^2$, $\rho = 7800 \text{ Kg/m}^3$, $\alpha = -1.28 \cdot 10^9 \text{ N/m}^2$, $\beta = 0.32 \cdot 10^9 \text{ N/m}^2$, $\xi = 220.90 \cdot 10^9 \text{ N/m}^2$, $H_0 = 100 \text{ A/m}$, $Jk^2 = 1$, $\Omega = 50/\text{s}$.

Using Snell's law, the angle of reflections and the wave numbers are calculated. Also the speeds of waves; c_1 , c_2 , c_3 and c_4 for qlD, qTD, qTM and the wave due to voids, respectively, are obtained from quartic Eq. (3.3). Thus, the graphs are presented in Figs. 2-4. That is, we considered variations of rotation Ω (angular velocity) of the medium, magnetic field, and voids ξ parameters. This is to ascertain the effects of these parameters on the horizontal reflection coefficients (RC or Z_i) of the reflected waves when, in particular, the P-wave is incident with angle e .

Figures 2a-2d represents the effects of rotation to the reflection coefficients Z_i , $i = 1, 2, 3, 4$ of the waves (qlD, qTD, qTM and due to voids) under constant magnetic fields and voids parameters. Also it suffices that the reflection coefficients have its maximum close to the normal incidence angle of the wave in the medium. Consequently, Figs. 2a-2d depict that the reflection coefficients increase when the rotation parameter increases. Though, the reflection coefficients in Figs. 2a-2d show very slight uniform behavior near $e > 40^\circ$ as it vanishes at grazing angles of incidence. Moreover, an increase in the angle of incidence, decreases the reflection coefficients in all cases due to reinforcement of the medium. However, it entails that the propagation of waves at different points in the medium with an increase in rotation will decrease the speed of waves

except for the wave due to voids (Fig. 2f), which is unaffected at all points of propagation. Also, as the angle of propagation increases, the speed of waves increases. The speed of waves vanishes at the grazing angle of incidence, which is the same for the coefficients of reflected waves. Hence, the dependencies of the constituent parameters of the system are proportional.

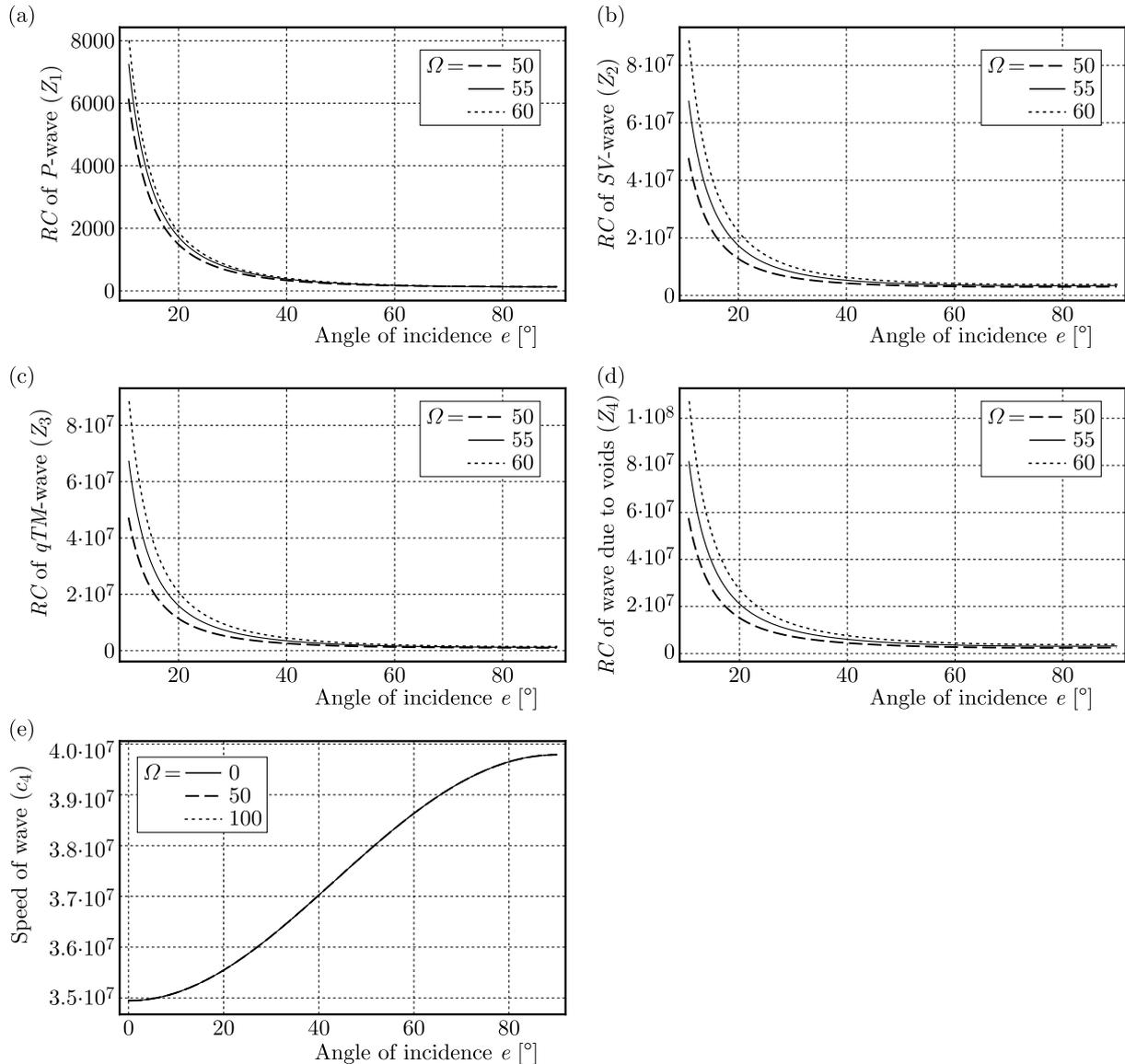


Fig. 2. Variations of the reflection coefficients Z_i and speed of waves versus the incidence angle for distinct values of rotation Ω

It is observed in Figs. 3a-3d that the reflection coefficients $Z_i(RC)$, $i = 1, 2, 3, 4$ of qLD (P-wave), qTD (SV-wave), qTM (quasi-transverse microrotational wave) and wave due to voids, respectively, decrease for the increasing angle of incidence for uniform rotation and voids parameters. They have sharp and fast increasing behavior in the presence of constant rotation and voids effects with respect to varying high magnetic field H_0 effects, except for Z_3 which decreases. In Fig. 3 $Z_i(RC)$, $i = 1, 2, 3, 4$ start with their curves at maximum values close to the normal incidence and, afterwards, decrease slightly when the angle of incidence varies near $e > 45^\circ$ and, finally, vanish at grazing incidence. Thus, at some points in the medium, varying magnetic field effects could lead to a decrease or increase in the reflection coefficients of the waves with combined uniform porosity and rotation of the medium. Furthermore, for higher

magnetic field, reflection of the wave is possible and its reflection coefficients may possess small or high values in such a medium. Thus, for an increased incidence angle, reflection coefficients in the micropolar fibre-reinforced medium yield low values in the presence of rotation and voids.

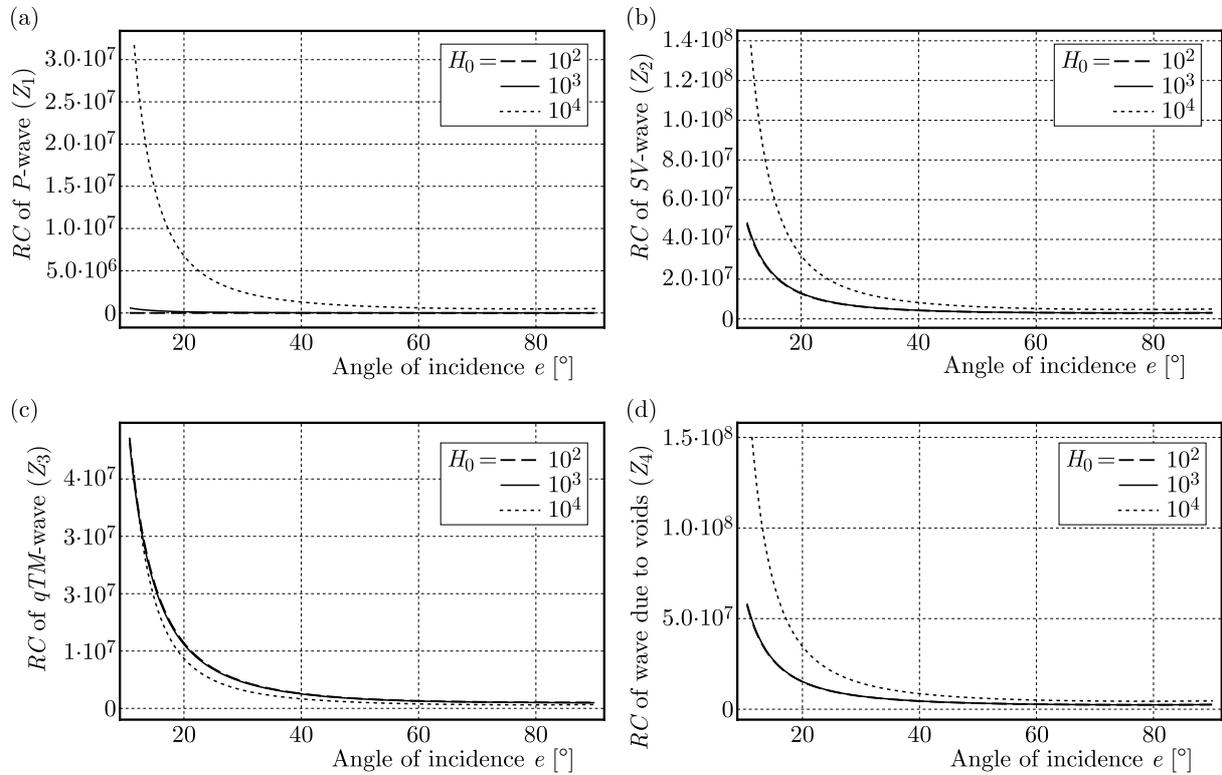


Fig. 3. Variations of the reflection coefficients Z_i versus the incidence angle for distinct values of H_0

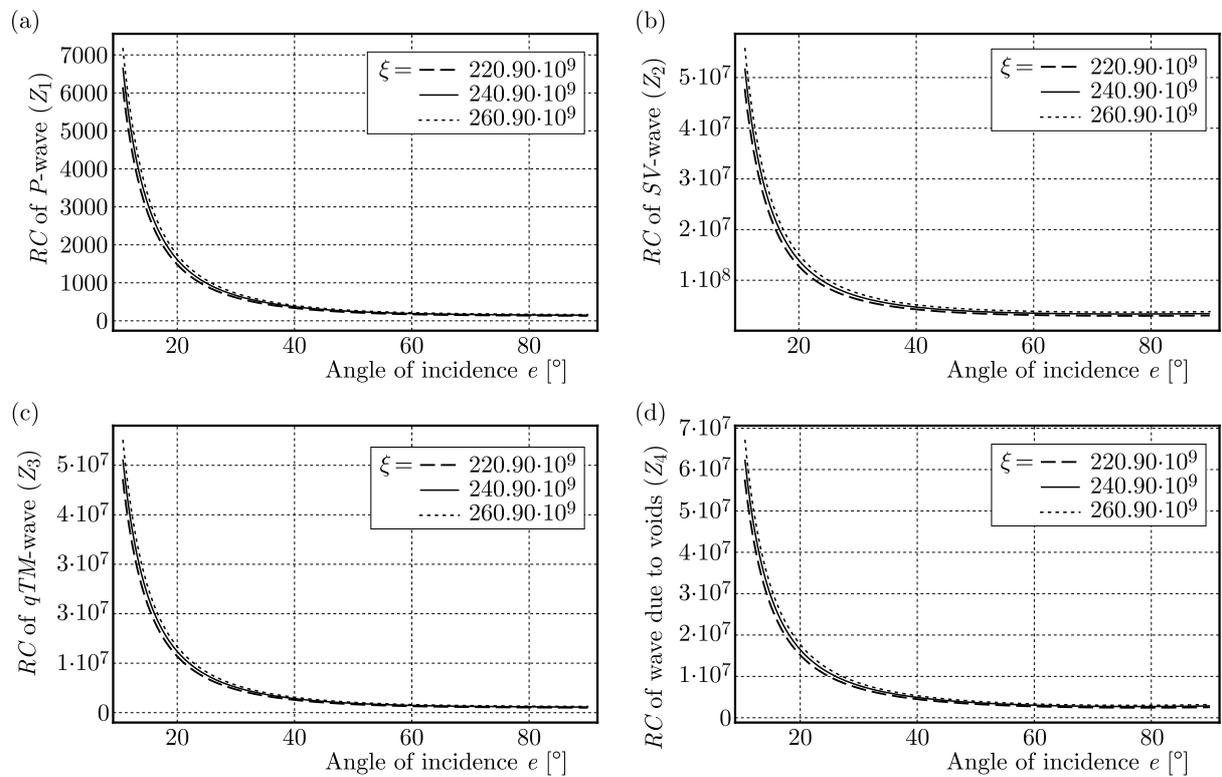


Fig. 4. Variations of the reflection coefficients Z_i versus the incidence angle for distinct values of ξ parameter

Furthermore, Figs. 4a-4d depict variation of reflection coefficients $Z_i(RC)$, $i = 1, 2, 3, 4$ of qLD (P-wave), qTD (SV-wave), qTM (quasi-transverse microrotational wave) and the wave due to voids, respectively, for uniform rotation and magnetic field parameters. They are increasing with respect to an increased voids parameter ξ in the presence of a constant applied magnetic field and rotation. They decrease when the angle of incidence increases due to the micropolar fibre-reinforced medium. Figure 4 shows the curves at maximum values close to the normal incidence and, subsequently, decreasing very slightly and finally vanishing at grazing incidence.

6. Conclusion

We investigated the propagation and reflection of magneto-elastic plane waves at free surfaces of a rotating micropolar fibre-reinforced medium with porosity. Four coupled reflected plane waves traveling in the medium; quasi-longitudinal displacement (qLD) wave, quasi-transverse displacement (qTD) wave, quasi-transverse microrotational (qTM) wave and a wave due to voids were observed. The characteristics of the propagation and reflection of the waves were made up of angular velocity of the medium Ω , micropolar fibre-reinforced and voids parameters under the influence of magnetic fields. It was deduced that these parameters greatly influenced the reflection coefficients Z_i , speeds and modulation of waves. It means that the micropolar fibre-reinforcement tends to decrease the reflection coefficients in the medium with effects of rotation, magnetic fields and voids as the angle of incidence increases in the medium. The speeds of waves were affected by the rotation parameter by decreasing its propagation. Generally, the reflection coefficients Z_i , decreased for an increased incident angle due to the micropolar fibre-reinforcement. It is noted that rotation increased at certain values the reflection coefficients while high magnetic field decreased the reflection coefficients Z_i of reflected qTM waves in the modelled problem. Moreover, voids increased the reflection coefficients of qLD, (P-wave), qTD (SV-wave) and qTM (quasi-transverse microrotational wave) and waves due to voids. Also it is deduced that reflection might not occur for certain incident angles in the medium. The method used in this study is noteworthy for dealing with such problems for successful investigation. Our modeled problem is similar to Sunita *et al.* (2019) if the magnetic field, micropolarity and voids are neglected in the presence of thermo-elasticity.

The investigation should prove to be helpful for new researchers in the field and experimental based study involving propagation and reflection of magneto-elastic plane waves at free surfaces of a rotating micropolar fibre-reinforced medium with voids and also in fields with similar models such as in optics, geophysics, design of new materials, etc.

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